

Another EMC resource from EMC Standards

Shield current induced noise is negligible

CCC

Audio-frequency shield current induced noise is negligible

(as long as it does not flow in the 0V system)



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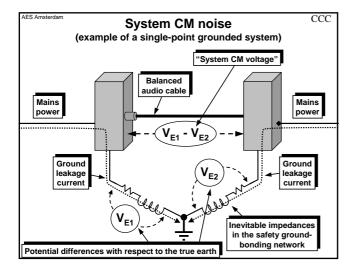
Audio benefits
from EMC installation techniques

- To meet the EMC directive, a number of large pro-audio systems have followed IEC 61000-5-2
 - with cable shields connected to chassis at both ends
 allowing 'ground loop' currents to flow in the shields
- These systems have been excellent for EMC
 - but have also been found to have improved audio performance over precious systems (S/N, bandwidth)
- This short presentation helps to explain why the audio performance is so good

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The origin of common mode (CM) noise in a system

- Systems have a number of items of equipment located in different places
 - so experiencing different ground (earth) potentials from each other
 - and interconnected by balanced shielded cables
- The balanced interconnect is intended to reject the "system CM noise"
 - the noise voltage that exists between the grounds of two items of interconnected equipment
 - but nothing is perfect

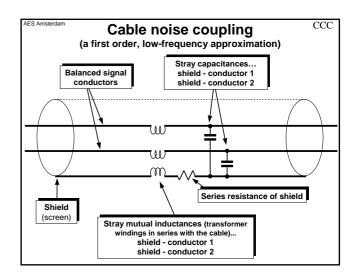


How should we connect
the shield of the balanced cable?

- We can choose to connect each cable's shield to the equipment at one end only, or at both ends
- Experience shows that good EMC performance and low levels of RF demodulation
 - and compliance with the EMC Directive (EN 55103-1 / -2)
 - is most easily achieved at lowest cost by direct (DC) shield bonding at both ends
 - + as recommended by IEC 61000-5-2
 - but how does this affect the amount of system CM noise that gets into the signal?

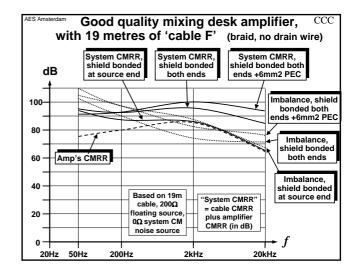
The system noise voltage couples from the shield to the signal conductors by...

- Stray capacitance, which causes a commonmode (CM) noise voltage
 - and the *imbalance* between the stray capacitances causes differential-mode (DM) noise voltage
- Stray mutual inductance
 - ◆ i.e. a 1:1:1 transformer (above some frequency)
 - causes a CM noise voltage (180° to capacitance noise)
 - and the *imbalance* between the stray mutual inductances causes a DM noise voltage



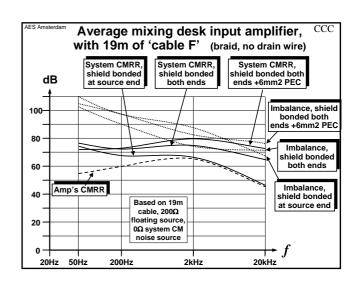
Implications for signal/noise (S/N) ratios

- The CM voltage on both of the signal conductors
 - is processed by the amplifier's CMRR and its gain, resulting in a DM noise
- The imbalance (DM) voltage between the signal conductors
 - is processed by amplifier gain as if it is wanted signal
- Here are some examples for a cable type "F"
 - showing the relative effects of each of the above noise contributions....



19m of 'cable F' with a *good* mixing desk amplifier

- Single-ended shield bonding at source
 - gives better system CM noise than would be expected from the amp's CMRR spec, below 2kHz
- Bonding shield at both ends makes system CM noise worse by up to 15dB above 300Hz
 - achieving >70dB overall, over the frequency range
- Both-ends-bonded plus 6mm² PEC makes system CM noise worse by up to 4dB above 1kHz
 - achieving >75dB overall, over the frequency range



19m of 'cable F' with an *average* mixing desk amplifier

- Single-ended shield bonding at source
 - gives better system CM noise than would be expected from the amp's CMRR spec, below 2kHz
- Bonding shield at both ends makes system CM noise better by up to 19dB, above 50Hz
 - achieving >65dB overall, over the frequency range
- Both-ends-bonded + 6mm² PEC makes system CM noise better by up to 28dB above 100Hz
 - achieving >70dB overall, over the frequency range

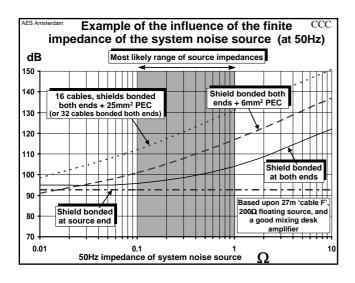
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But the system's voltage noise source does *not* have a 0Ω impedance

(as the previous graphs assumed)

- So bonding shields at both ends will reduce the source noise voltage
 - as will using using PECs
- Reducing both capacitive and inductive coupled cable noise (CM and DM)
- In a large system there can be >100 cables
 - and bonding all their shields at both ends has a very beneficial effect indeed on system CM noise rejection



Always connect the shield to the chassis. frame or enclosure shield

- It used to be common to connect shields to circuit 0V
 - now well-known to be very bad practice
 - because of 'common-impedance coupling'
- If the circuit's 0V reference is pure clean water...
 - then the shields are sewers
 - and their currents should never flow in the 0V

Why we don't let shield currents flow in the 0V any more

- Example: a 0.1" wide 0V trace just 1" long (in a 1oz copper printed circuit board)
 - has an impedance of $4.8m\Omega$ at 50Hz
- Just 25mV of 'system CM noise' at 50Hz creates a shield current of 100mA (in 19 metres of 'cable F')
- If this 100mA shield noise current was allowed to flow in the 1" long 0V trace...
 - it would create 480µV of 'common impedance noise' in the circuit's 0V reference system

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For a singer or violinist using a typical 200 Ω dynamic microphone...

- 480µV of noise in the 0V could result in a S/N ratio of 20dB
 - worse, where a number of signals share the noisy 0V
- Whereas S/N due to shield-coupled noise alone
 - would be 56dB for an average mixing desk amplifier, and 76dB for a good one (single cable, 0Ω noise source)
 - both much lower than the acoustic background noise for a microphone signal
 - for 16 cable shields in parallel: >66dB and >86dB likely

